



REC 2021  
May 17-20, 2021



# ***“Comparison of fully non-stationary artificial accelerograms generation methods in non-linear dynamic analyses”***

**Federica Genovese<sup>1,2</sup>, Giuseppe Muscolino<sup>2</sup> and Alessandro Palmeri<sup>1</sup>**



<sup>1</sup>*Loughborough University, United Kingdom*

<sup>2</sup>*University of Messina, Italy*



# INTRODUCTION

- **Non-linear dynamic analysis:** powerful tool to assess the performance of earthquake-resistant structural systems provided that key sources of non-linearity are accurately represented
- **Response:** highly sensitive to the way of modelling the **dynamic action**
- **Problem:** choice of proper sets of acceleration records to be used as input motion in Structural dynamic analyses

# INTRODUCTION

- **Literature:** different procedures for **selection of real accelerograms** applying large acceleration scale factors leading to unrealistic inputs
- The selection of a **set** of real accelerograms **compatible with the code requirements** applying large acceleration scale factors leads to unrealistic inputs

**Alternative:**  
**Artificial accelerograms**

# AIMS OF THE PAPER

- **Develop a new method** for generating fully non-stationary artificial accelerograms having the same characteristics of the target motion
- Investigate the **effect of different generation procedures** on the non-linear seismic response of structures



Proposed  
**wavelet based  
method (CWT)**



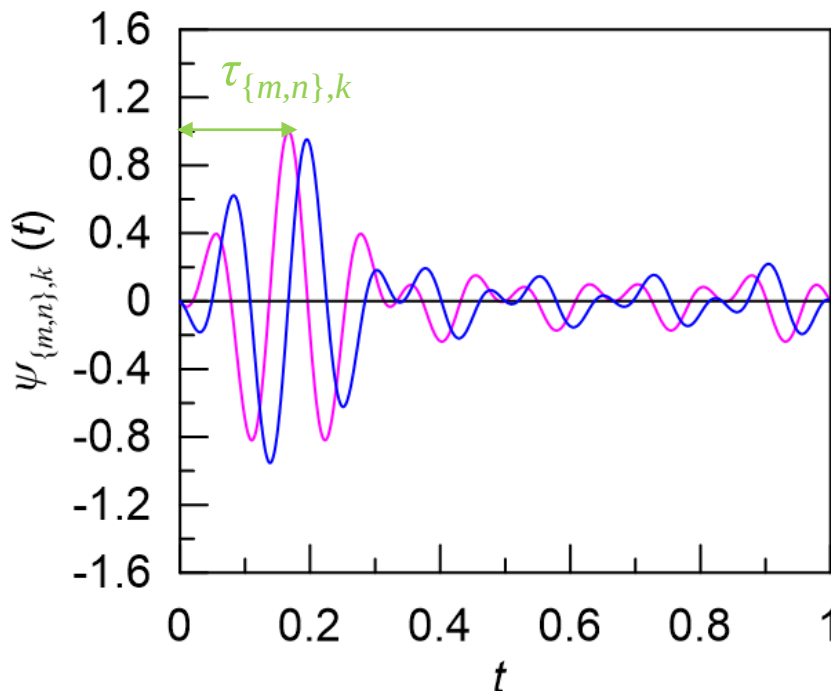
Evolutionary Power Spectral  
density (**EPSD**) function method  
(Muscolino et al. 2021)

# WAVELET BASED METHOD

Mother wavelet: **circular harmonic wavelet**

$$\omega_m = 2\pi m$$
$$\omega_n = 2\pi n$$

$$\psi_{\{m,n\},k}(t) = \frac{1}{n-m} \sum_{j=m}^{n-1} \exp \left[ i \omega_j (t - \tau_{\{m,n\},k}) \right]$$

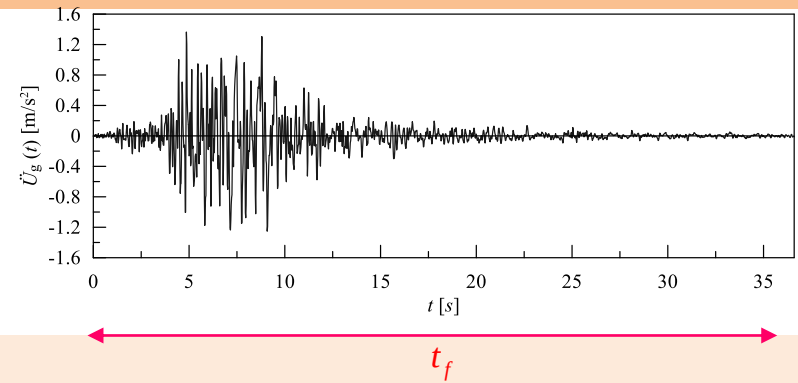


$$\tau_{\{m,n\},k} = k / (n - m)$$

— Real part  
— Imaginary part

# STEPS: WAVELET BASED METHOD

1) Select a Target signal  $\ddot{U}_g(t)$



2) Evaluate the Harmonic Wavelets Transforms Coefficients

$$a_{\{m,n\},k} = (n-m) \sum_{\ell=0}^N \ddot{U}_g(t_{\ell}) \cdot \frac{\Delta t}{t_f} \cdot \bar{\psi}_{\{m,n\},k} \left( \frac{t_{\ell}}{t_f} \right)$$

R.V.  
[0, 2\pi]

3) Apply the proposed **randomization formula**

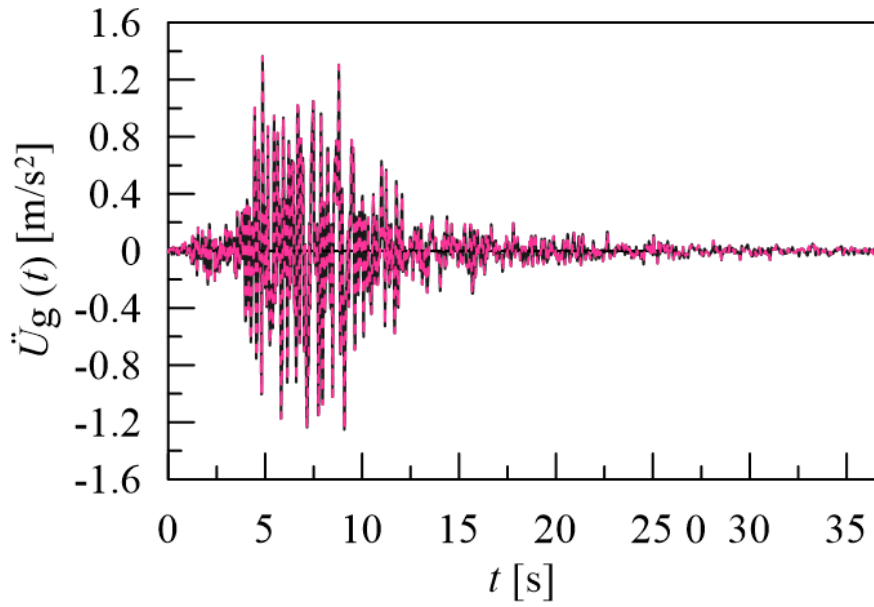
$$f^{(i)}(t) = 2 \sum_{\{m,n\}} \sum_{k=0}^{n-m-1} \sum_{j=m}^{n-1} \frac{|a_{\{m,n\},k}|}{n-m} \times \cos \left[ i 2 \pi j \left( \frac{t}{t_f} - \tau_{\{m,n\},k} \right) + \theta_{\{m,n\},k} + \phi_{\{m,n\},k}^{(i)} \right]$$

$$\theta_{\{m,n\},k} = \arg \left\{ a_{\{m,n\},k} \right\}$$

# STEPS: WAVELET BASED METHOD

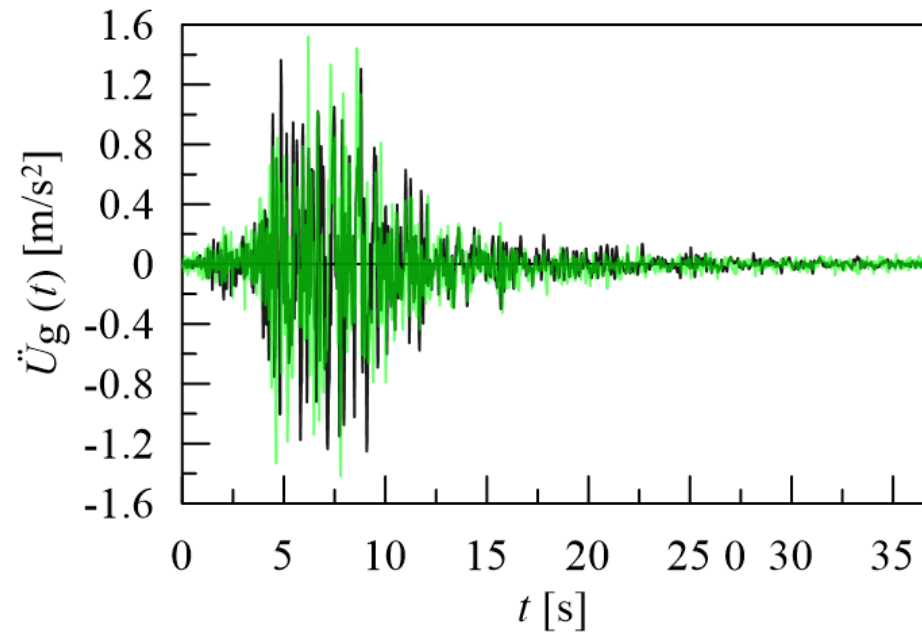
$$f^{(i)}(t) = 2 \sum_{\{m,n\}} \sum_{k=0}^{n-m-1} \sum_{j=m}^{n-1} \frac{|a_{\{m,n\},k}|}{n-m} \times \cos \left[ i 2 \pi j \left( \frac{t}{t_f} - \tau_{\{m,n\},k} \right) + \theta_{\{m,n\},k} + \phi_{\{m,n\},k}^{(i)} \right]$$

$$\phi_{\{m,n\},k}^{(i)} = 0$$



Original signal

$$\phi_{\{m,n\},k}^{(i)} \neq 0$$

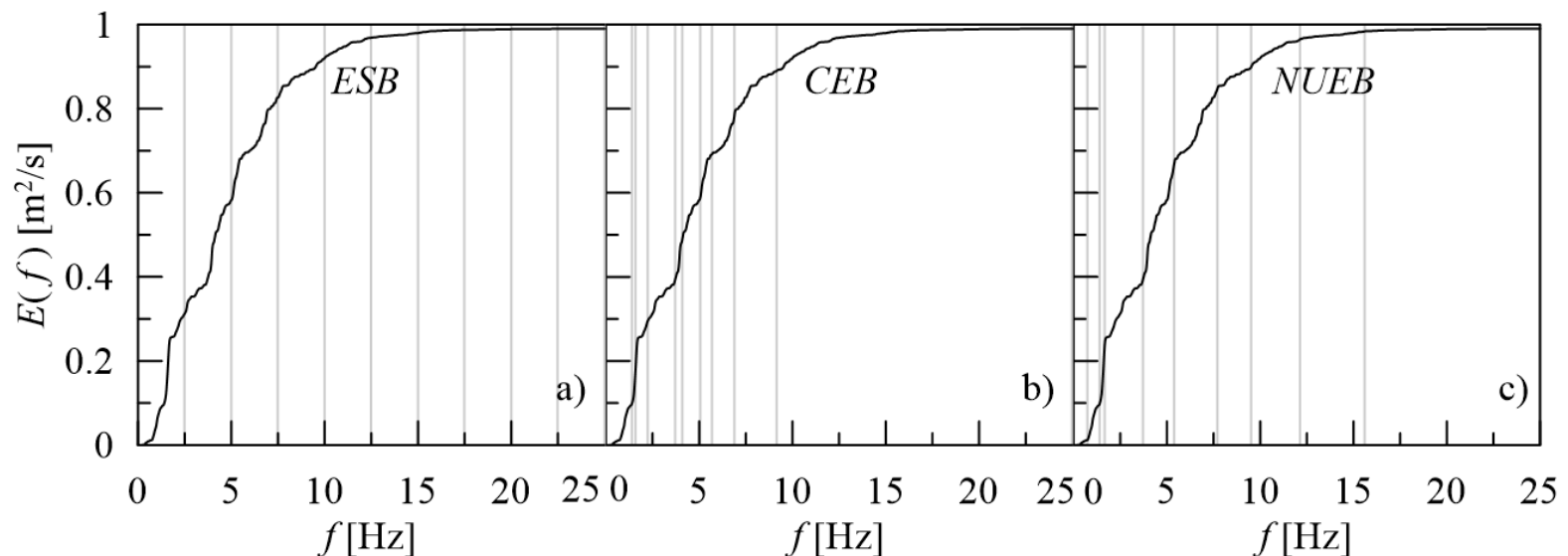


$i$ -th sample

# FREQUENCY DOMAIN SUBDIVISION

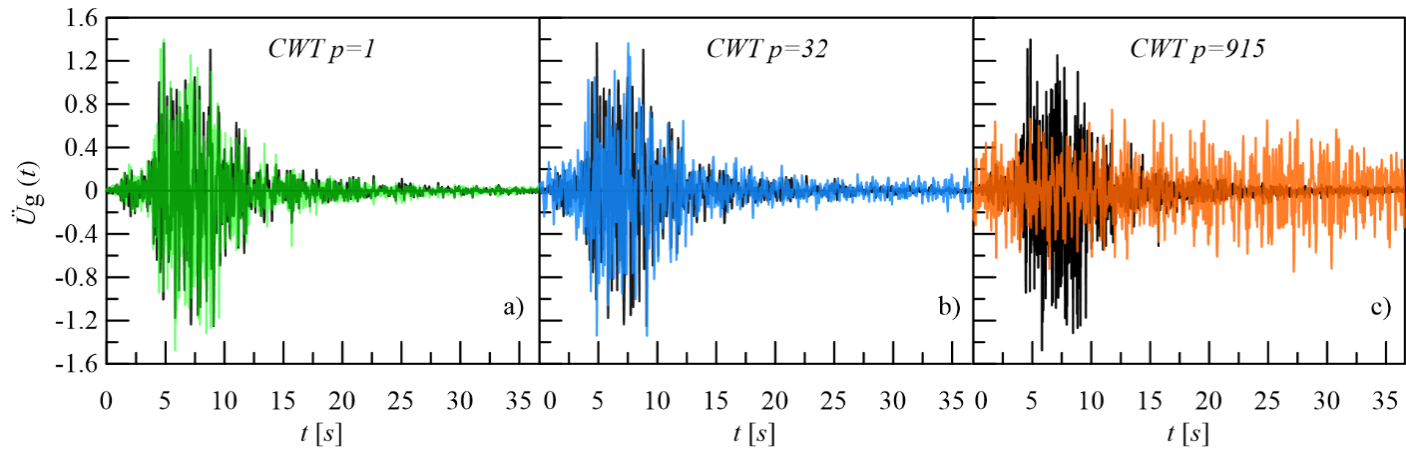
- 1) equal-spaced bandwidths (*ESB*)
- 2) constant energy bandwidths (*CEB*)
- 3) non-uniform energy bandwidths (*NUEB*)

$$E(f) = \int_0^{f_c} (|\mathcal{F}[\ddot{U}_g(t)]|)^2 df$$

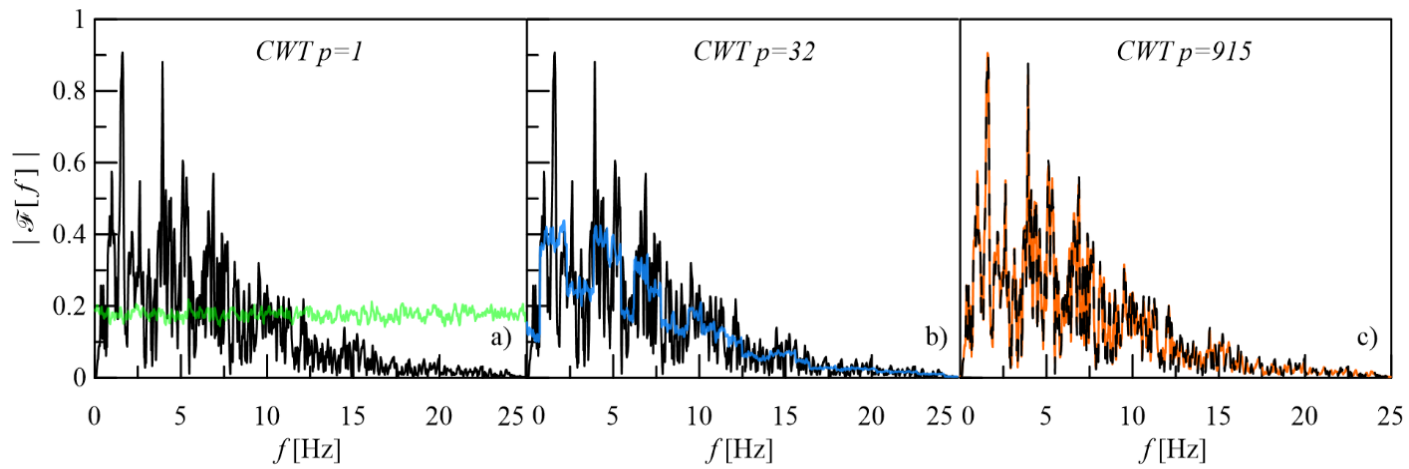


# THREE *ESB* SCHEMES

## Time histories

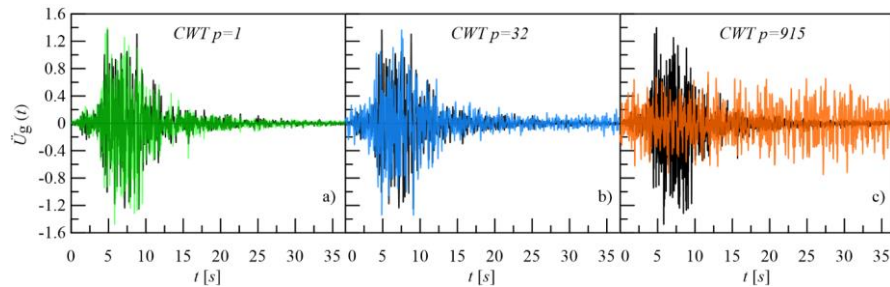


## Fourier spectra

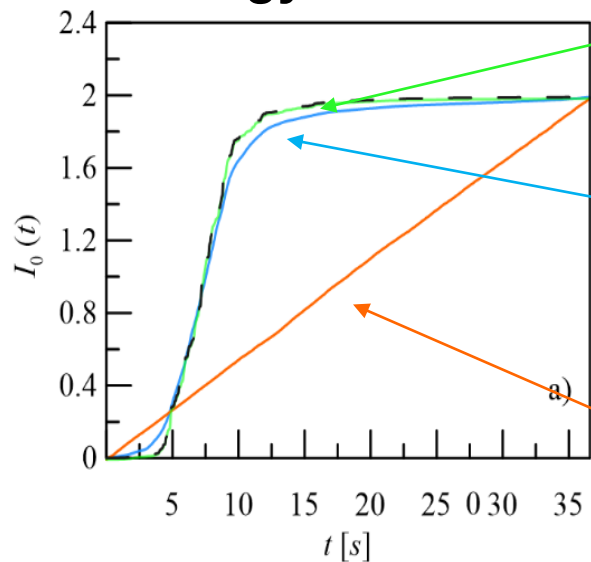


# THREE *ESB* SCHEMES

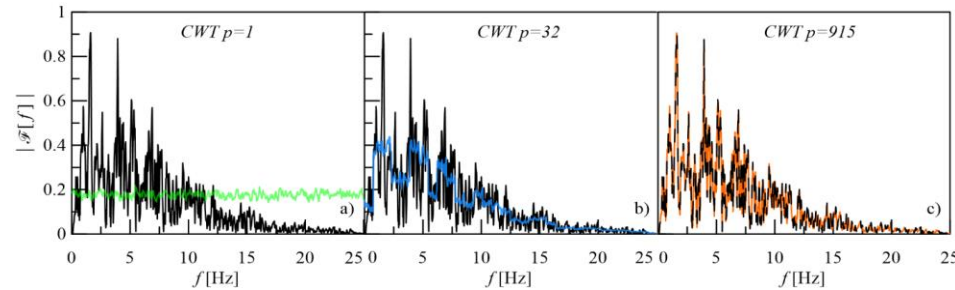
## Time Domain



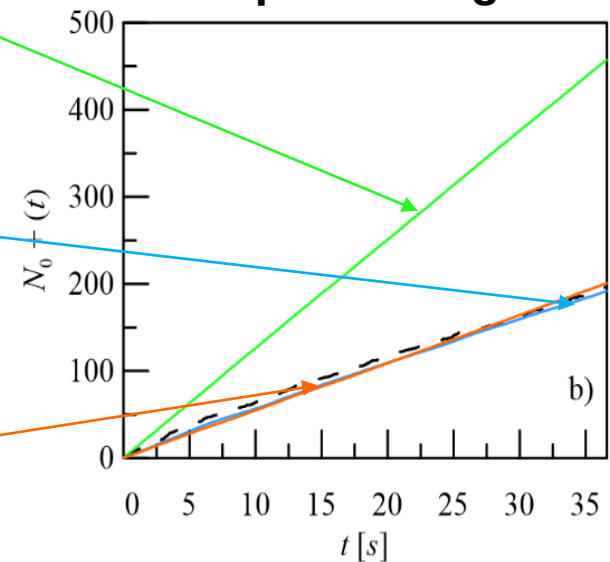
## Cumulative Energy functions



## Frequency Domain



## Cumulative Zero-level up-crossing functions

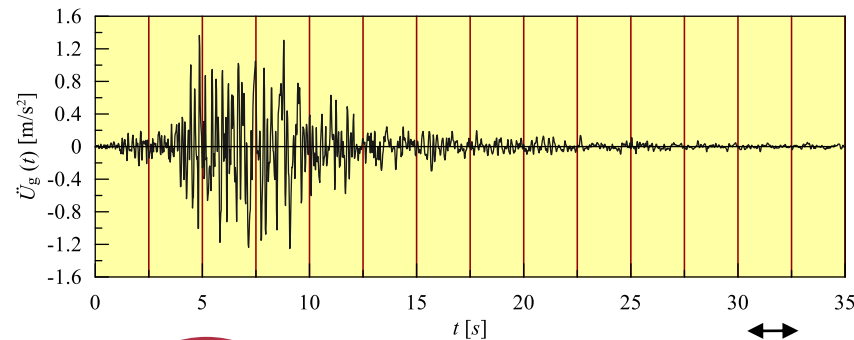


# EPSD METHOD

(Muscolino G., Genovese F., Biondi G. and Cascone E., Soil Dynamics 2021)

## Four steps procedure:

- 1) Subdivide a Target signal in many time intervals



$$F_0(t) = \sum_{k=1}^n F_{0,k}(t) = \sum_{k=1}^n a(t) X_k(t) \mathcal{W}(t_{k-1}, t_k) \quad \Delta T_k$$

Fully non stationary process

Uniformly modulated random process

Modulating function

Stationary subprocess

$$G_{X_k}(\omega) = \beta_k \left( \frac{\omega^2}{\omega^2 + \omega_{H,k}^2} \right) \left( \frac{\omega_{L,k}^4}{\omega^4 + \omega_{L,k}^4} \right) \frac{\rho_k}{\pi} \left( \frac{1}{\rho_k^2 + (\omega + \Omega_k)^2} + \frac{1}{\rho_k^2 + (\omega - \Omega_k)^2} \right); \quad k = 1, \dots, n$$

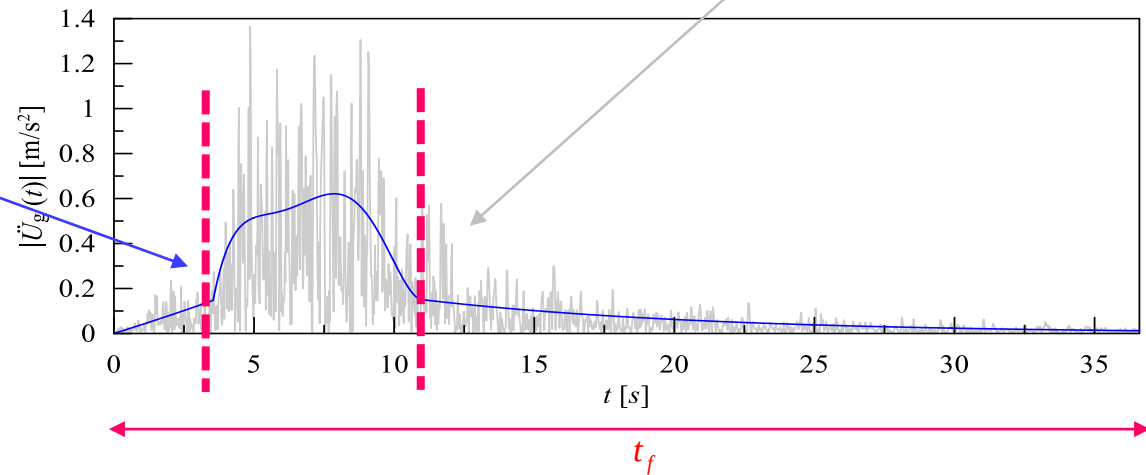
# EPSD METHOD

(Muscolino G., Genovese F., Biondi G. and Cascone E., Soil Dynamics 2021)

## 2) Estimate modulating function

$$a(t) = \sum_{j=1}^2 \bar{a}_j(t) \mathbb{W}(t_{j-1}, t_j) + a(t_2) \exp \left[ \frac{t - t_2}{t_f - t_2} \ln \left( \frac{|\ddot{U}_g(t_f)|}{a(t_2)} \right) \right] \mathbb{W}(t_2, t_f)$$

$a(t)$



## Optimization problem

$$\left\{ \begin{array}{l} \text{find } \alpha_1, \alpha_2, \dots, \alpha_p; \\ \text{minimising } \int_{t_{j-1}}^{t_j - \Delta t} \left[ E_{\ddot{U}_g}(t) - \psi_j(t) \right]^2 dt; \quad j = 1, 2 \\ \text{such that } \bar{a}_j(t) \geq 0, \quad \bar{a}_j(t) = \sum_{i=1}^p \alpha_i (t - t_{j-1})^i, \quad t_{j-1} \leq t < t_j; \end{array} \right.$$

$$E_{\ddot{U}_g}(t) = \int_0^t \ddot{U}_g^2(\tau) d\tau = \sum_{j=1}^{m \leq n_a} \int_{t_{j-1}}^{t_j} \ddot{U}_g^2(\tau) d\tau$$

$$\mathbb{E} \langle E_{F_0}(t) \rangle = \int_0^t \mathbb{E} \langle F_0^2(\tau) \rangle d\tau = \sum_{j=1}^{m \leq n_a} \int_{t_{j-1}}^{t_j} a^2(\tau) d\tau = \sum_{j=1}^{m \leq n_a} \psi_j(t) = \sum_{j=1}^{m \leq n_a} \int_{t_{j-1}}^t \left[ a(t_{j-1}) + \bar{a}_j(\tau) \right]^2 d\tau$$

# EPSD METHOD

(Muscolino G., Genovese F., Biondi G. and Cascone E., Soil Dynamics 2021)

## 3) Fully non-stationary samples

$$F_0^{(i)}(t) = a(t) \sqrt{2\Delta\omega} \left[ \sum_{k=1}^n \sum_{r=1}^{m_N} \mathbb{W}(t_{k-1}, t_k) \sin(r \Delta\omega t + \theta_r^{(i)}) \sqrt{G_{X_k}(r \Delta\omega)} \right]$$

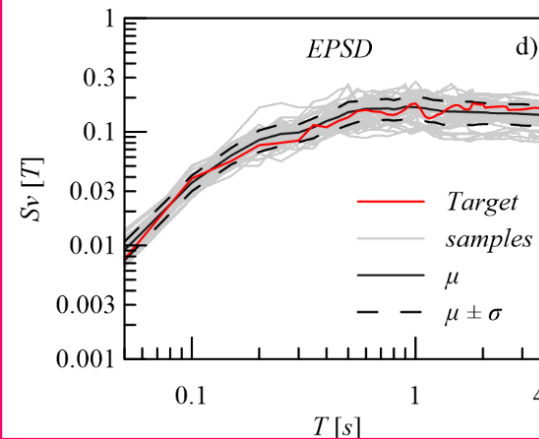
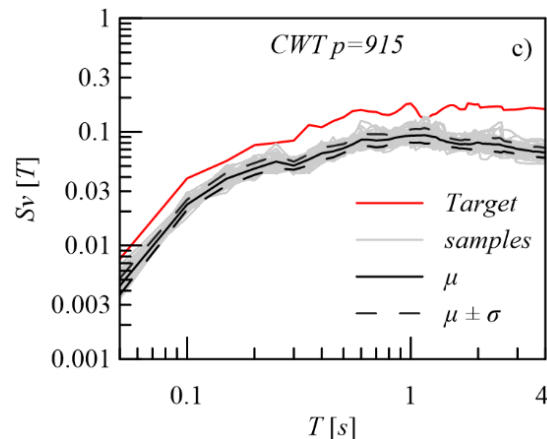
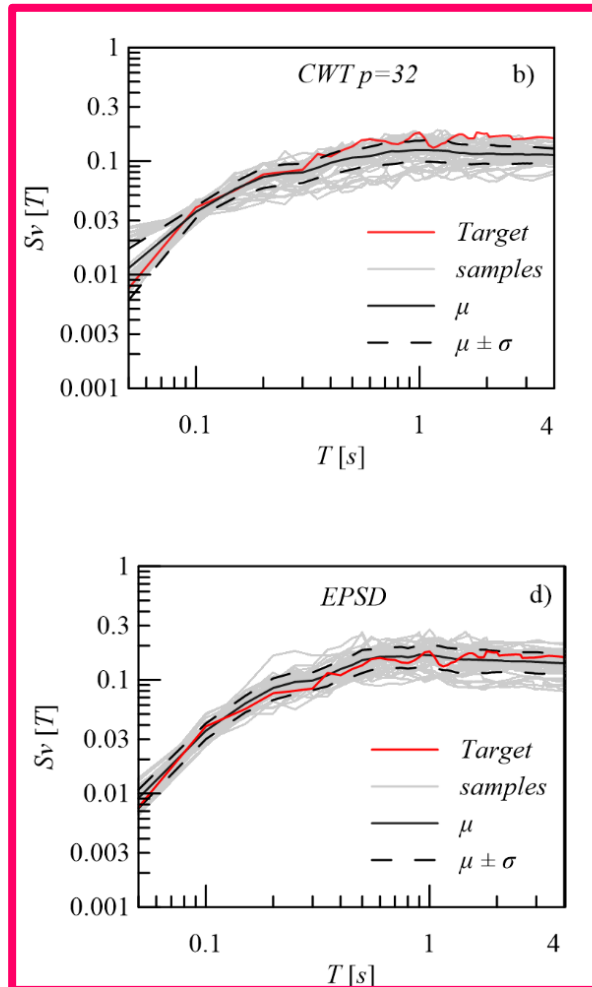
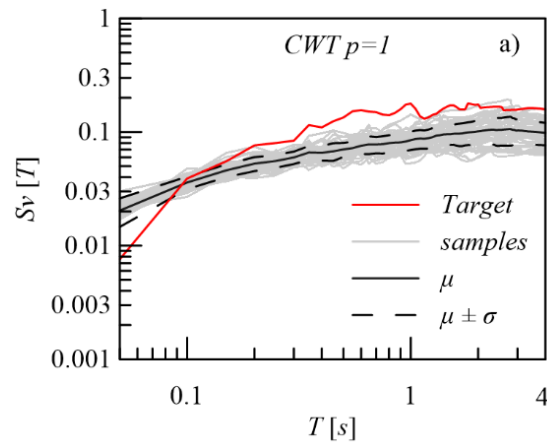
## 4) Fully non-stationary samples spectrum compatible artificial accelerograms ( $j$ -th iteration)

$$\bar{F}_0^{(i,j)}(t) = a(t) \sqrt{2\Delta\omega} \left[ \sum_{k=1}^n \sum_{r=1}^{m_N} \mathbb{W}(t_{k-1}, t_k) \sin(r \Delta\omega t + \theta_r^{(i)}) \sqrt{\bar{G}_{X_k}^{(j)}(r \Delta\omega) G_{X_k}(r \Delta\omega)} \right]$$

$$\bar{G}_{X_k}^{(j)}(r \Delta\omega) = \bar{G}_{X_k}^{(j-1)}(r \Delta\omega) \frac{S_e^{(T)}(r \Delta\omega, \zeta_0)^2}{\bar{S}_e^{(j-1)}(r \Delta\omega, \zeta_0)^2}$$

# COMPARISON

## CONSTANT-DUCTILITY RESPONSE SPECTRA



# CONCLUSIONS

- Two fully non-stationary artificial accelerograms generation methods have been compared
- The *CWT*-method, allows generating the samples without the need of defying the *EPSD* function
- The *EPSD* function method allows to obtain samples with characteristics closer to the target event than those generated with *CWT* method (*ESB*) but tends to be more complex and requires several iterative steps